AMENDMENTS TO THE SPECIFICATION:

Paragraph numbers referenced below are those used in published application US Patent Application Publication No. 2006/0128496.

Prior to paragraph [0001], insert the following headings:

BACKGROUND

1. Field

Between paragraph [0001] and paragraph [0002], insert the heading:

2. Description of Related Art

Replace paragraph [0002] with the following paragraph:

[0002] ~~Such~~ An embodiment of a golf club head is described ~~known~~ e.g. in ~~from~~ published US patent application 20020045490. At least the strike surface of the golf club head illustrated there, which has a hollow construction, is made of a precipitation-hardened, corrosion-resistant maraging steel with a martensite temperature M_s > 130 °C. An embodiment of the ~~The~~ maraging steel described there has a chromium content of 10.0 to 12.5 ~~11.5~~ wt.%, a molybdenum content of 1.5 to 2.5 wt.% and nickel content of 8.5 to 10.5 wt.%, a titanium content of 1.2 to 1.6 wt.%, a boron content of 0.001 to 0.005 wt.%, and carbon, nitrogen, silicon, and manganese contents of 0.1 wt% or less, provided that C + N = 0.015 wt.%, the rest being iron. This maraging steel is precipitation-hardened by the ~~a~~ titanium content of 1.2 to 1.6 wt.% of titanium. An alloy of vanadium serves as a carbide- and/or nitride

catcher. With this maraging steel, a tensile strength of more than 1700 MPa can be achieved.

Between paragraph [0004] and [0005], insert the heading:

SUMMARY

Between paragraph [0009] and [0010], insert the heading:

BRIEF DESCRIPTION OF DRAWING

Between paragraph [0010] and [0011], insert the heading:

DETAILED DESCRIPTION

Between paragraphs [0015] and [0016], insert the following paragraph:

In a particular embodiment, the maraging steel consists essentially of 8.0 wt.% nickel, 13.0 wt.% chromium, 0.2 wt.% titanium, 0.25 wt.% beryllium, 1.0 wt.% molybdenum, the rest being iron together with unavoidable impurities.

Replace paragraph [0016] with the following:

[0016] To correctly adjust the components for the alloy melt, it has been found that the martensite temperature M_s, which must be above 130 °C. according to the present invention, can be adjusted by equation (1):

$M_s = [629.45 - \underline{16.8}\ \cancel{6.8}(Cr + 1.2\ Mo + 0.6\ W) - 24.5(Ni + 0.15\ Co) - 13.2\ Mn - 11.2\ Si - 670(C+N)]$ °C (1)

Replace paragraph [0020] with the following:

[0020] The melt is then poured into a mold. The ingots from the present alloys are then bloomed at a temperature of approximately 1000 °C. to 1200 °C. and are then hot formed into a strip at ~~100~~ 900 °C ≤ T_1 ≤ 1150 °C. Low heat rolling temperatures are chosen to minimize the edge zones depleted of free beryllium.

Replace paragraph [0025] with the following:

[0025] In an advanced embodiment of the present invention, this heat treatment is followed by another heat treatment at 300 °C ≤ T_4 ≤ 470 °C, more particularly at 350 °C ≤ T_4 ≤ 470 °C. This heat treatment is carried out for 10 to 100 hours. Due to this additional special heat treatment it is possible to obtain particularly high tensile strengths R_m of approximately 2800 MPa.

Replace paragraph [0027] with the following:

[0027] Furthermore, yield strengths $R_{p0.2}$ > 2100 MPa can be obtained at the same time. In the case of the special second heat treatment, yield strengths $R_{p0.2}$ > 2500 MPa, more particularly $R_{p0.2}$ > 2600 MPa, can be achieved.

Replace paragraph [0029] with the following:

[0029] In addition, the maraging steels in accordance with the invention exhibit, due to the high strengths, an extremely high storable energy R_m^2/E-modulus ~~modulo~~ of ~~approximately~~ more than 30 MPa and in special cases of approximately 40 MPa, which is particularly advantageous for use as a strike surface. Moreover, the basic materials in turn exhibit very low damping values, which is attributed to the high

strengths and very fine martensitic structure in which the size of the grains lie in the range of approximately 1 μm.